THE INFLUANCE OF GARLIC (Allium sativum) OIL AS QUANCHING MEDIUM FOR HEAT TREATMENT OF PLAIN CARBON STEEL.

Sani. A. Salihu

Abstract

In this work, the garlic oil was evaluated as an alternative quench medium for hardening of plain carbon steel. The steel was heated to 860°C and socked for an hr, quenched and tempered separately in water and garlic oil. The mechanical properties (strengths, hardness, impact and ductility) of plain carbon steel (0.42%C) were investigated under two different quenching media (water and garlic oil). The investigations centered on water and garlic oil quenched and tempered conditions (300°C, 350°C, 400°C and 450°C). The results show that tensile strength of 2706.8 N/mm² was obtained from sample quenched and tempered at 300°C in water, while garlic oil gave lowest tensile strength value of 1906.9 N/mm² when tempered at 450°C but the highest impact strength of 28 J. .The highest hardness value of 52.2 HRA was obtained from the sample quenched in water and tempered at 300°C, while the lowest hardness value of 41.6 HRA was also obtained from sample quenched in garlic oil and tempered at 450°C. There were variations in microstructure of tempered samples from the two quenchants used in this study. The tensile strength and hardness values were decreasing while impact strength and ductility appreciably increase with increasing of tempering temperature due to the decomposition of martensite. Result indicated that water quenched steel produced its best properties in strength and hardness, while garlic oil quenched steel has its best property in impact strength and ductility.

Keywords: Microstructure, Martensite, Tensile Strength, Hardness, Quenchants

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INTRODUCTION.

Steel is one of the most commonly used materials in industrial applications due to its low cost, high strength, and durability. Steel can be define as an alloy of iron and carbon usually containing between 0.015% 2.14% carbon, often with other to constituents such as manganese, silicon, sulphur, phosphorus (Gulyev, 1984. Higgins, 1995). Plain carbon steels are widely used for many industrial applications and manufacturing because of their low cost and easy fabrication (Smith and Hashemi 2006). They are classified on the basis of their carbon content as their major alloying element is carbon into low carbon steel, medium carbon steel and high carbon steel. According to Rajan et al. (1988), steels with carbon content varying from 0.25% to 0.65% are classified as medium carbon, while those with carbon content less than 0.25% are termed low carbon. The carbon content of high carbon steels usually ranges within 0.65-1.5%. Hardness and other mechanical properties of plain carbon steels increase with the rise in concentration of carbon dissolved in austenite prior to quenching during hardening heat treatment (Rajan et al. 1988; Thelning 1984), which may be due to transformation of austenite into martensite (Feng and Tahir 2008).

The choice of correct quenching medium plays an important role in determining the desire properties of engineering materials. The basic function of a quench medium is to control the rate of heat transfer from the surface of the part being quenched (Kulikov, 1997, Higgins, 2001). Accordingly, many components use oil quenching to achieve consistent and repeatable mechanical and metallurgical properties and predictable distortion patterns. The reason oil quenching is so popular is due to its excellent performance results and stability over a broad range of operating conditions. Oil quenching facilitates hardening of steel by controlling heat transfer during quenching, and it enhances wetting of steel during quenching to minimize the formation of undesirable thermal and transformational gradients which may lead to increased distortion and cracking. Therefore, the mechanical strength of medium carbon steels can be improved by quenching in appropriate medium. However, the major influencing factors in the choice of the quenching medium are the kind of heat treatment, composition of the steel, the sizes shapes of the and parts (Rassizadehghani et al. 2006). As explained by Grishin and Churyukin (1986), mineral oils have been found to exhibit best cooling

capacity for the majority of alloy steels but they are relatively expensive, toxic and nonbiodegradable.

Currently, vegetable oils are one of the most commonly identified renewable, biodegradable and non-toxic quenchants. In addition to their relatively narrow viscosity range, vegetable oils exhibit considerably lower thermal-oxidative stability relative to petroleum oil, which has been a significant factor inhibiting its use in the industry. As an alternative to mineral oil, vegetable oils are used as quench media. They are cheap, available. abundantly biodegradable, renewable environment and friendly (Tagaya and Tamura, 1954). There is an increasing interest in the use of vegetable oils as renewable, biodegradable and nontoxic alternatives to petroleum oil-based quenchants for the heat treating industry. One of the first commercial references to the use of vegetable oil as a metal quenchant was a patent issued in 1932 (Tagaya and Tamura, 1954). More recently, the use of locally available vegetable oils, which are relatively cheap. non-toxic and environmental friendly, as quenching media, has begun to generate attention (Ndaliman 2006).

In the present work, garlic oil is used as quenchant to study its effectiveness. Its widespread availability and low cost make garlic oil an ideal component for developing renewable, bio-based products.. After heating the steel it is quenched and tempered in tap water and one biodegradable quenchant i.e. garlic oil and tested for various mechanical properties.

2.0 RESEARCH METHODOLOGY

Sample of plain carbon steel bar with 16 mm diameter and 2 m long was purchased from a local

market located at Jega, 50 kilometers away from Birnin Kebbi, Northern, Nigeria. The chemical composition of material under investigation is given in Table 1 while Table 2 is the physicochemical properties of garlic oil. Standard tensile and impact specimens were made from steel sample using lathe according to AISI standard. machine Samples were subjected to hardening, and tempering at four different tempering temperatures and were tested for tensile, yield, percentage elongation, hardness and impact toughness. Each test was conducted three times and the average taken represents the results recorded in Table 3.

| Element | C | Mn | Si | S | Р | Fe |
|-------------|------|------|------|-------|-------|-----|
| Composition | 0.42 | 0.63 | 0.37 | 0.001 | 0.002 | Bal |
| (wt, %) | | | | | | |

Table 1. Chemical composition of steel used

Table 2. Some physicochemical properties of oils used

| Туре | Colour | Specific | Viscosity | Flash | Iodine | Free fatty | Boiling | Saponificati |
|--------|-----------------|----------|--------------------|-------------------|--------|------------|-------------------|--------------|
| of oil | | gravity, | at 40° C, | point, | value | acid, | point, | on value |
| | | (g) | (poise) | (⁰ C) | | (% Oleic | (⁰ C) | (MgKOH/g) |
| | | | | | | acid) | | |
| Garlic | Light yellow | 0,95 | 0.098 | 145 | 12.73 | 2.10 | 140 | 193 |

2.1 Heat Treatment

Generally heat treatment is accomplished in three stages: Stage I—Heating the samples slowly to ensure a uniform temperature. Stage 2—Soaking (holding) the samples at a given temperature for a given time. Stage **3**—Cooling the samples to room temperature (Rajan et al 1988). Specimen for heat treatment and subsequent hardness, impact and tensile testing were obtained from 20 mm diameter bar of a 0.42%C medium carbon steel. A muffle furnace was used for austenitizing the specimens at 860° C for 1 hr and then quenched separately in tap water and garlic oil. Then the specimens were subjected to tempering heat treatments, within the temperature range of 300-450°C. After which the hardness, impact and tensile properties were determined in as tempered state using Rockwell hardness tester, Charpy impact tester and universal tensile testing machine respectively.

2.2 Mechanical Test

2.2.1 Tensile Testing

Tensile test were carried out on the quenched specimens using Instron Universal Tester. Each

of the specimens was loaded till fractured, and the fracture load for each sample was recorded as well as the diameter at the point of fracture and the final gauge length. The initial diameter and initial gauge length for each sample was noted before the application of the uniaxial load. The percentage elongation of each test sample was determined, as well as the tensile strength.

2.2.2 Hardness Test

For hardness testing, oxide layers formed during heat treatment were cleaned and polished. Rockwell hardness method was used for the determination of the hardness of the quenched and tempered samples. The specimens were brought in contact with the pyramid indenter and allowed to rest for a dwell time. The hardness of the specimens were indicated by the penetration of the indenter on the test specimens, and displayed by the machine. Average values were recorded after repeating the test for each of the test specimens.

2.2.3 Impact Test

Heat-treated samples were tested for various mechanical properties. Impact energy was

recorded using the Charpy impact tester. Charpy V-notch specimens were machined from tempered rod, in the ASTM standard form of 10mm×10mm×55mm. Both tensile, hardness and impact data reported in this work are the average values of the data obtained from steel samples. All testing was done in accordance with ASTM standard test procedures (ASM, 2008).

3.0 Results and discussion

The tensile, hardness and impact tests were performed at room temperature and the results of tensile, hardness, impact and percentage elongation tests are presented in Table 3. As observed, the both the ultimate tensile strength and hardness decrease with increase of tempering temperature for both quenchants. However, the impact strength and percentage elongation increase with increase of tempering temperature.

| Quenchant | Heat treatment | Tensile | Yield | Hardness, | Impact | Percentage |
|------------|-----------------------|-------------------|-------------------|-----------|-------------|-------------|
| | | strength, | strength, | HRA | strength, J | Elongation, |
| | | N/mm ² | N/mm ² | | | % |
| Garlic oil | Quenched at 860°C and | | | | | |
| | tempered at 300°C | 2457 | 1942 | 51.3 | 18 | 9 |
| | Quenched at 860°C and | | | | | |
| | tempered at 350°C | 2173 | 1894 | 45.2 | 19 | 12 |
| | Quenched at 860°C and | | | | | |
| | tempered at 400°C | 1906 | 1696 | 41.6 | 23 | 15 |
| | Quenched at 860°C and | | | | | |

Table 3. Mechanical Properties of various samples used

| | tempered at 450°C | 1732 | 1512 | 36.3 | 28 | 19 |
|-------|------------------------------------|--------|--------|------|----|----|
| | | | | | | |
| Water | Quenched at 860 [°] C and | 2706.8 | 2369.4 | 53.2 | 11 | 1 |
| | tempered at 300°C | | | | | |
| | Quenched at 860°C and | 2385.3 | 2046.6 | 51.3 | 13 | 3 |
| | tempered at 350°C | | | | | |
| | Quenched at 860°C and | 2178.9 | 1798.4 | 48.5 | 17 | 6 |
| | tempered at 400°C | | | | | |
| | Quenched at 860°C and | 1954.2 | 1635.2 | 45.9 | 19 | 8 |
| | tempered at 450°C | | | | | |

3.1 Microstructure.

Metallographic examination was carried out on the medium carbon steel specimens. Standard techniques for specimens preparation for the microstructure observation were adopted. The samples were mounted on bakelite using silicon carbide abrasive papers (240 to 600 grits sizes). Following the polishing of specimens on a rotating disc and subsequent surface cleaning, etching of the polished specimen was done using 2% Nital (2% Nitric acid, HN0₃, in ethyl alcohol) for 15-30 seconds to develop the structure. The structures obtained were photographed, and are shown in Figure 1.

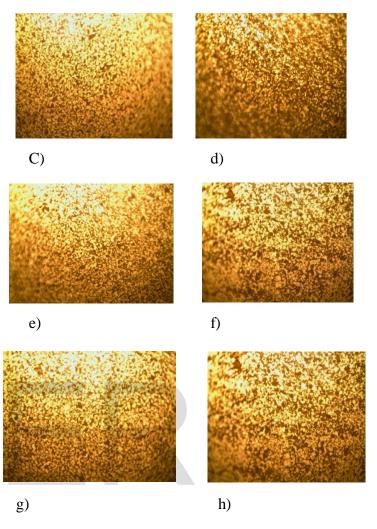
3.1.1 Effect of quenching media on microstructure and mechanical properties

The quenching media under investigation have shown an effect on the microstructural formation and mechanical properties of the steel because of their different

physicochemical properties. Figure 1 (a). shows the microstructure of the as-received medium carbon steel which reveals the presence of ferrite, pearlite and inclusions. As explained by Novikov, (1980), different quenching media have significant role in determining the final structure of an alloy because of different cooling rates. The quenching media under investigation have different cooling rate. Of the quenching media under investigation, water is the most severe and garlic oil the least. Figure 1 shows microstructures of two specimens that underwent the same heat treatment conditions, but with different quenching media. The results of structural formations show different proportions of martensites, retained austenite and carbides. Figure 1 also show that with increase of tempering temperature, structural transformations were observed revealing more bainitic structure,

less retained austenite for samples tempered in garlic oil and martensite more especially with samples that were tempered at 300 to 350° C in water.

When the tempering temperature is higher than 350° C the cementite in the tempered martensite coarse as explained by Lakhtin, (1977). With an increase in the tempering temperature the carbon concentration of the matrix in the tempered martensite still decreases due to the diffusion of carbon atoms to the cementite. The strength of the tempered martensite decreases and its ductility increases (Senthilkumar and Ajiboye, 2012). Therefore, the ultimate tensile strength of the tempered ferritemartensite decreases and its elongation increases as observed by Senthilkumar and Ajiboye, (2012), and Ashish Vermaa, Pravin Kumar Singh, (2013). When the specimens (garlic oil) are tempered at temperature 450°C, phase transformation takes place from retained austenite to bainite. Bainitic structure consist of ferrite and epsilon carbide which are formed at temperature ranging between 400°C-450°C.





i)





b)

IJSER © 2014 http://www.ijser.org Figure 1. Microstructures of quenched and tempered showing the distribution of tempered carbides: a) as-quench; shows pearlite in matrix ferrite, b) QWT; 300⁰C, c) QOT; 300⁰C, d) QWT; 350⁰C, e) QOT; 350[°]C, f) QWT; 400[°]C, g) QOT; 400[°]C, QWT; 450[°]C, QOT; 450[°]C

(QWT means quenched in water and tempered, while QOT is quenched in oil and tempered).

TABLE 4: Microstructure of Quenched and Tempered Steel in Two Quenchants

| QUENCHING MEDIA AND TEMPERING TEMPERATURE | MICROSTRUCTURE |
|--|--|
| Untreated sample | Ferrite (white) and pearlite (dark) |
| Water - 300° C (QWT) | Ferrite (white) and coarse carbide (dark) |
| Water -350° C (QWT) | ferrite (white) and coarse carbide (dark) |
| Water -400° C (QWT) | ferrite and coarse tempered martensite |
| Water -450° C (QWT) | Consists of an equilibrium coarse mixture of |
| | ferrite (white) and carbide (dark) |
| Garlic oil – 300° C (QOT) | Fine tempered martensite plus ferrite |
| Garlic oil – 350° C (QOT) | Consists of coarse tempered martensite and |
| | bainite |
| Garlic oil -400° C (QOT) | Coarse tempered martensite and bainite |
| Garlic oil - 450° C (QOT) | Tempered martensite and bainite |

3.2 Mechanical properties

3.2.1 Ultimate tensile strength.

Fig. 2 shows the variation of ultimate tensile strength (UTS) of the garlic oil and tap water as a function of tempering temperature. At 300°C, sample quenched in garlic oil displayed tensile strength of $2457/\text{mm}^2$, while tap water exhibited highest tensile strength value of 2706.8 N/mm². At 350°C, all the quenched and tempered samples gave lower tensile strength value, with sample quenched in garlic oil showing lowest tensile strength value because of the formation of tempered martensite. However, at 400°C and 450°C, heat treated samples quenched in garlic oil displayed slight decrease of tensile strength because of decomposition of martensite.

The effect of tempering temperature on yield strength is illustrated in Fig. 3. Yield

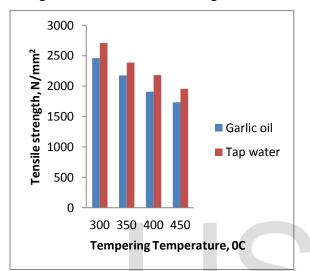


Fig. 2. Effect of tempering temperature on ultimate tensile strength for different quenchants

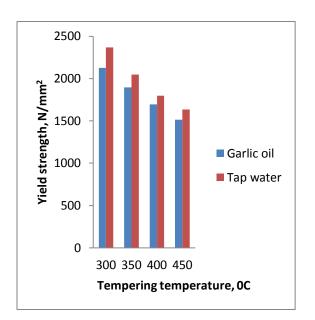


Fig.3 Effect of tempering temperature on yield strength for different quenchants

Strength responded to the tempering temperature in same manner with Tensile Strength. Yield Strength continuously decreased with increasing tempering temperature for both samples quenched and tempered in garlic oil and water.

3.2.2 Variation of the hardness of the tempered samples

The hardness property of tempered specimens is measured as function of tempering temperature using Rockwell hardness tester. The results obtained from testing of specimens quenched at 860°C and tempered at temperature 300, 350, 400 and 450°C was shown in Fig. 4. There are two different significant trends in this graph because of changing of structural effect. The highest Rockwell hardness value of the samples quenched in tap water and garlic oil were obtained at 300°C, with peak value from the sample quenched in tap water, as shown in Figure 4. However, at 350°C, the hardness values of water the quenched sample decreased slightly, with those quenched in garlic oil became lower than that of the as-received sample, which is 42.3 HRA. The hardness values of all the samples increased at 300°C above that of the asreceived, but later decreased when quenched after heating up to 450°C. Moreover, the resulting tempered structures are expressed

in Figure 1b to 1i. According to these microstructures, bainitic structure (ferrite and epsilon carbide) are formed at 400°C to 450°C. This indicates that the best heating temperature to obtain highest hardness value will be 300°C with garlic oil as quenching medium. There was decrease in hardness

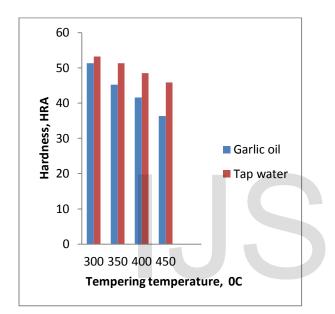


Fig. 4. Variation of hardness against tempering temperature for different heat treatments

because of the formation of tempered martensite and bainite and structure when tempered in garlic oil, while the tempered samples quenched in tap water experienced slight decrease.

3.2.3 Impact properties

The mechanical properties of tempering samples (tempered at 300°C, 350°C, 400°C and 450° C) showed that the Toughness in J increases with increase of tempering temperature. The results of the specimens which were hardened with tap water and garlic oil quenched and then tempered at 300° C, 350° C, 400° C and 450° C are expressed graphically in Figure.5. Impact toughness responds to tempering temperature in the similar manner to percentage elongation.

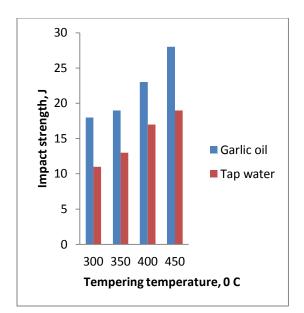


Fig. 5 Effect of tempering temperature on impact strength of specimens tempered in different quenchants.

4.0 Conclusions

The following conclusion has been drawn from the experimental result and discussion already made.

1. The results show that the ultimate tensile strength and the yield strength decrease, whereas the elongation and impact strength increase with increase in tempering temperature.

2. Ultimate tensile strength decreases continuously by increasing tempering temperature. The ductility of the specimen is measured by the tensile test. The elongation increases with the increase in tempering temperature. 3. The heat treatment of steel using garlic quenchant gives the better mechanical properties and microstructure by forming ferrite and epsilon carbide at 350°C to 400°C, hence garlic oil stands as a potential quenching medium in heat treatment of steel.

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